

# Dynamically self-adjustable liquid-liquid and self-adaptive soft-contact solid-solid triboelectric nanogenerator for wave energy harvesting

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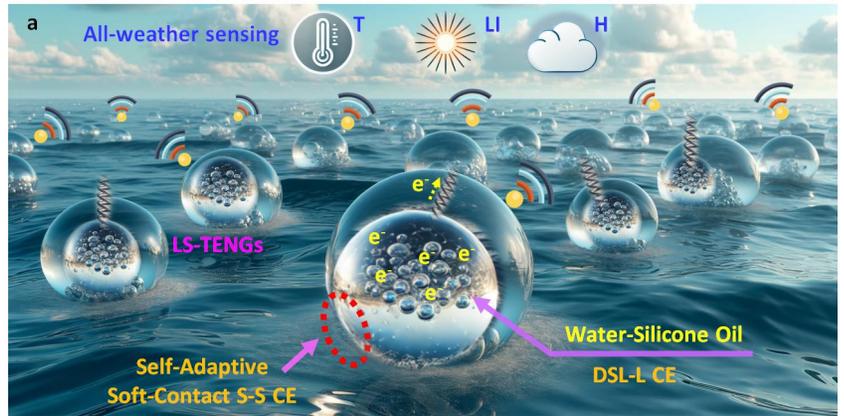
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The paper presents a novel ellipsoidal, pendulum-like triboelectric nanogenerator (LS-TENG) that integrates both liquid-liquid (L-L) and solid-solid (S-S) triboelectric effects, designed for efficient wave energy harvesting and continuous, self-powered marine environment monitoring. The innovative structure, with dynamically self-adjustable L-L interfaces and self-adaptive soft S-S contacts, significantly enhances energy harvesting efficiency and protects the device from mechanical wear, offering a promising solution for sustainable energy generation in marine environments.

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## ABSTRACT

Water wave energy exhibits great potential to alleviate the global energy crisis. However, harvesting and utilizing wave energy are challenging due to its irregularity, randomness, and low frequency. Triboelectric nanogenerators (TENGs) have gained significant attention for harvesting wave energy with high efficiency. This study presents a novel ellipsoidal, pendulum-like TENG integrating both liquid-liquid (L-L) and solid-solid (S-S) triboelectricity (LS-TENG). This innovative design enables continuous wave energy harvesting and self-powered marine environment monitoring under various conditions, including temperature, humidity, and light intensity. The binary immiscible liquids within the LS-TENG's inner soft balloon create dynamic, and self-adjustable L-L contact interfaces, significantly increasing the L-L contact area and enhancing L-L contact electrification (CE). The unique self-adaptive, soft S-S contact increases the S-S contact area compared to traditional hard point contact, better adapting to the irregular movements of waves and promoting efficient S-S CE. The LS-TENG achieves highly efficient wave energy harvesting by coupling L-L and S-S CE. Furthermore, the unique soft contact design protects the S-S interfaces from mechanical wear and damage during long-term work. The LS-TENG's novel structure provides an innovative and effective way for water wave energy harvesting.

## KEYWORDS

self-adaptive, soft-contact, solid-solid, liquid-liquid, self-adjustable, triboelectric nanogenerator

## 1 Introduction

The escalating global energy demand and the environmental influence of traditional fossil fuels have intensified the search for sustainable and renewable energy sources [1-3]. Among the various renewable energy options, water wave energy, as a clean and inexhaustible energy resource, stands out due to its inherent characteristic of being abundant, predictable, and consistent, which can alleviate the global energy crisis [2, 4-9]. However, despite its potential, effectively harvesting and harnessing wave energy remains a challenge. This is primarily due to unresolved technological issues and the high costs associated with energy harvesting. Additionally, the irregular and low-frequency nature of ocean waves complicates the energy conversion process, making it difficult to capture energy efficiently [2, 5, 10-14].

Triboelectric nanogenerators (TENGs) [10-13, 15], based on the expanded Maxwell's displacement current as the underlying physical mechanism and with the polarization density term  $P_s$  in the electrical displacement vector as its central element [16, 17], have emerged as a novel solution to these challenges which are mainly employed to harvest energy from irregular and low-frequency mechanical motions, consequently well-suitable for ocean wave energy harvesting

[12, 18-27]. Although recent progress based on new materials and novel TENG devices, even including artificial intelligence (AI) for future TENG materials and devices, is emerging [28-32], traditional TENGs designed for water wave harvesting are typically spherical structures that utilize rigid S-S point contact [33-38]. This type of configuration still results in several problems, such as limited point contact areas and insufficient contact-separation dynamics, leading to inefficient energy harvesting [37]. Besides, the physical structure of these spherical TENGs is always too complicated to fabricate, and the adaptability of the internal parts to water wave motions is quite limited [1, 26, 39-42]. More importantly, the S-S interface's hard contact can easily cause mechanical wear and potentially damage the TENG devices, leading to water leakage. Additionally, these issues seriously hinder the practical application and longevity of TENGs in marine environments [38, 43-47].

To address the above problems of conventional TENGs for water wave energy harvesting, in this study, we design a novel ellipsoidal and pendulum-like structured TENG that integrates both L-L and S-S contact electrification (CE) (LS-TENG), enabling continuous harvesting of wave energy and self-powered monitoring of the marine environment under all weather conditions, including temperature (T), humidity (H),

1 and light intensity (LI) (Figure 1a). The structure of the  
 2 LS-TENG mainly consisted of the outermost hard spherical  
 3 shell and the internal cotton-covered soft liquid balloon system,  
 4 which is hung and balanced in the liquid balloon's inner  
 5 chamber via a copper core spring (Cu-spring), and takes on an  
 6 ellipsoidal shape due to gravity (Figure 1b). In the balloon, two  
 7 kinds of immiscible liquid were injected as the binary liquid  
 8 electrodes. This innovative structural design integrated both  
 9 L-L and S-S interface triboelectric effects during the LS-TENG's  
 10 working process to significantly enhance the wave energy  
 11 harvesting efficiency.

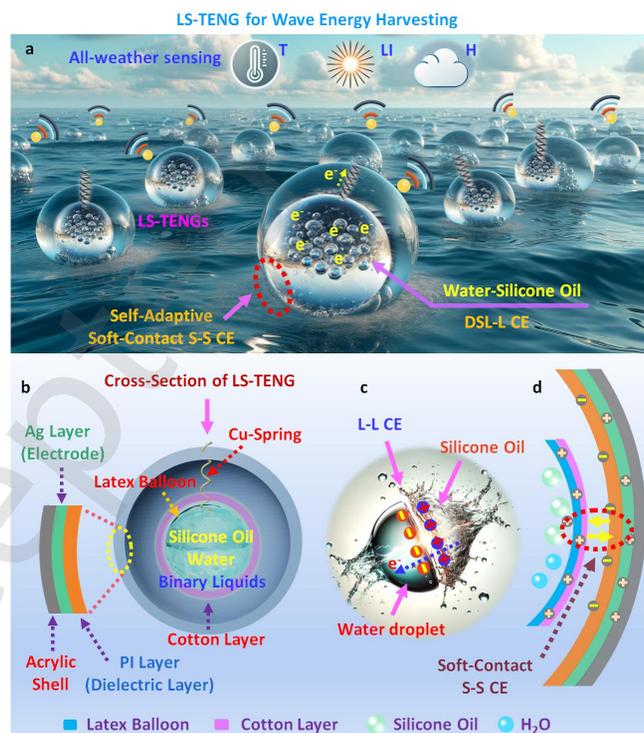
12 The soft liquid balloon adapts dynamically to the irregular  
 13 motions of water waves, enabling a unique self-adaptive and  
 14 soft contact with the inner surface of the external hard  
 15 spherical shell. This adaptation significantly increases the S-S  
 16 contact area [37], which can not only boost energy harvesting  
 17 efficiency but also play a crucial role in reducing mechanical  
 18 wear and extending the TENG's operational lifespan. The  
 19 introduced immiscible binary liquid electrodes in the inner soft  
 20 balloon create large numbers of dynamic self-adjustable L-L  
 21 contact interfaces when driven by the movement of water  
 22 waves, significantly increasing the L-L contact area, thus  
 23 promoting the transfer of triboelectric charge generated  
 24 between L-L interfaces and enhancing the efficiency of wave  
 25 energy harvesting (Figure 1c) [17, 48, 49]. Besides, this  
 26 spring-driven approach provides a quick and thorough S-S  
 27 contact-separation process and effectively facilitates the  
 28 separation of generated triboelectric charges, promoting wave  
 29 energy harvesting efficiency. Furthermore, we reasonably  
 30 proposed the triboelectric charge transfer mechanism at the  
 31 dynamic self-adjustable L-L contact interface by comparing the  
 32 LS-TENG's output performances based on different kinds of  
 33 immiscible binary liquid electrode systems. Additionally, by  
 34 enabling the LS-TENG to continuously harvest water wave  
 35 energy, self-powered monitoring of marine environments  
 36 under all weather conditions is successfully realized,  
 37 demonstrating the LS-TENG's promising potential in harvesting  
 38 and utilizing wave energy. The development of the LS-TENG  
 39 represents a significant advance in wave energy harvesting.

## 40 2. Results and Discussion

### 41 2.1 Structure of the LS-TENG.

42 The structure of the fabricated LS-TENG mainly consists of two  
 43 parts: an external transparent hard acrylic spherical shell and  
 44 an internal soft liquid latex balloon covered with a cotton layer  
 45 (Figure 1b). Regarding the external acrylic spherical shell, a  
 46 layer of silver, acting as one of the electrodes, was coated on the  
 47 inner surface of the hard acrylic spherical shell by magnetron  
 48 sputtering. Then, a polyimide tape is adhered to this silver layer  
 49 to serve as a dielectric layer. The optical image of the device  
 50 shows the silver layer uniformly coated on the inner surface of  
 51 the acrylic shell (Figure S1). As for the second part, the  
 52 preparation process of the internal soft liquid balloon can be  
 53 seen visually in Figure S2. Firstly, a copper core spring is  
 54 inserted into the latex balloon. Then two kinds of immiscible  
 55 liquids, silicone oil and deionized water, are injected into the  
 56 balloon as the binary liquid electrodes to make the balloon

bulge. Then, a thin cotton layer covers the outside of the liquid  
 balloon to serve as one of the S-S contact interfaces. The entire  
 liquid balloon system is securely suspended within the inner  
 cavity of the external hard acrylic spherical shell through the  
 copper core spring, which not only can transport the L-L  
 triboelectric charges but also allows for the adaptive and  
 responsive movement of the internal soft liquid balloon system  
 inside the hard spherical shell. The other end of the copper  
 core spring passes through the tiny hole in the rigid acrylic ball  
 shell to connect with the external circuit.



**Figure 1.** Wave energy harvesting and marine environment monitoring used by the LS-TENG and its structure and fabrication process. a) The wave energy harvesting and continuously self-powered all-weather monitoring of marine environments, including temperature (T), light intensity (LI) and humidity (H). b) Cross-section of the LS-TENG showing its interior structural details. c) The transfer of triboelectric charge generated between the L-L interfaces. d) The unique self-adaptive and soft contact manner between the S-S contact interfaces.

The inner soft liquid balloon, the key component of our LS-TENG, is fabricated from a commercial latex balloon that is robust, elastic, flexible, and chemically stable. These inherent advantages are vital for facilitating an adaptive ability to the dynamic deformation of the liquid balloon driven by the moving water waves. The dynamic self-adjust of the soft liquid balloon's shape can significantly increase the contact-separation area between the cotton layer and the inner surface of the hard acrylic spherical shell and facilitate the S-S triboelectric charge generation. Additionally, the exterior of the liquid balloon is coated with a cotton layer, serving as the counter-electrification layer. The entire balloon assembly is then securely mounted and suspended within the confines of the outermost hard spherical shell by a copper-core spring. This spring is integral to the LS-TENG, promoting an adaptive and responsive movement of the internal soft liquid balloon system relative to the rigid outer shell. The use of copper for the spring is due to its excellent electrical conductivity,

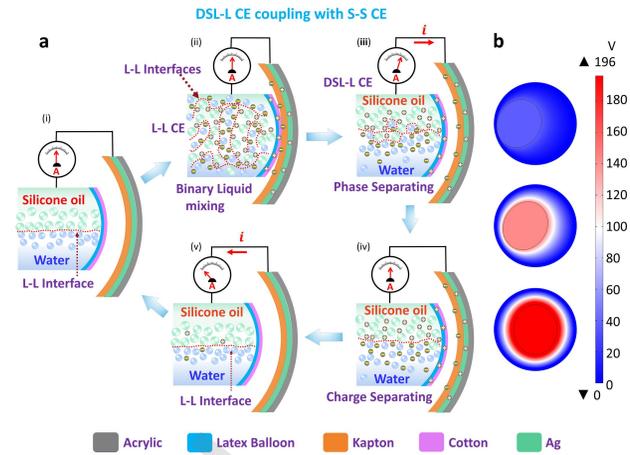
1 mechanical strength, and, crucially, its elasticity, ensuring  
2 consistent performance under varying mechanical movements.

3 With respect to the binary immiscible liquid electrodes in the  
4 inner soft balloon, the combination of silicone oil and deionized  
5 water was employed. When these two immiscible phases were  
6 mechanically forced to mix caused by the working LS-TENG's  
7 swinging movements, plenty of transient generated dynamic  
8 L-L contact interfaces would be created, which significantly  
9 increases the L-L contact area, thereby increasing the  
10 triboelectric charges generated at the interface of the two  
11 phases. During the dynamic movement of the LS-TENG, the  
12 immiscible liquids (silicone oil and deionized water) within the  
13 soft liquid balloon are constantly in motion, leading to frequent  
14 contact and separation at their interfaces. This motion  
15 generates triboelectric charges due to the difference in  
16 electronegativity between the two liquids. As these two phases  
17 contact and then separate, a charge transfer occurs at the  
18 interface. The generated charges are not confined to the liquid  
19 interface but are transferred to the copper core spring, which is  
20 connected to the external circuit. This spring serves as a  
21 conductive pathway, allowing the charges to move from the  
22 liquid interface inside the soft liquid balloon to the external  
23 circuit. Once the triboelectric charges are transferred through  
24 the copper spring, they flow into the external circuit,  
25 contributing to the LS-TENG's electrical output. This  
26 continuous process of charge generation, accumulation, and  
27 transfer ensures efficient wave energy harvesting (Figure 1c).

28 Moreover, the unique self-adaptive and soft contact manner  
29 additionally increased the S-S contact area (Figure 1d),  
30 enhancing energy harvesting efficiency and protecting the  
31 LS-TENG device from mechanical wear and damage. Figure S3  
32 exhibits the SEM images of the polyimide dielectric layer  
33 surface after different working periods (0 h, 6 h, 12 h, and 48  
34 h), demonstrating little mechanical wear on the contact  
35 surfaces and effectively extending the TENG's working  
36 longevity. The unique structure of the LS-TENG provides an  
37 innovative and effective way of collecting wave energy.

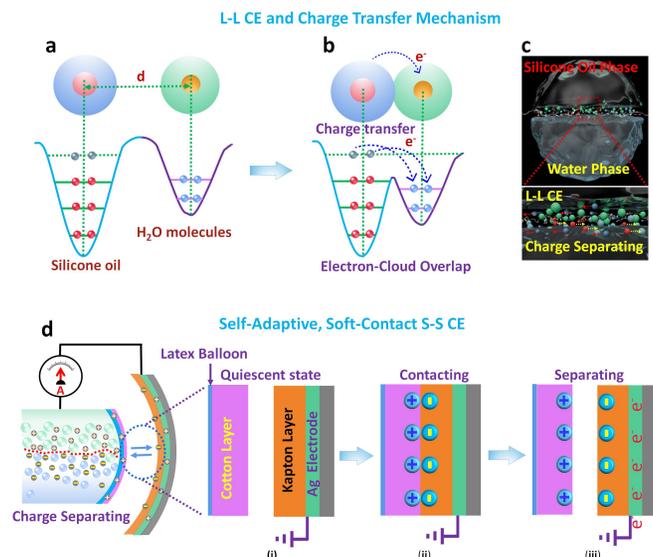
## 38 2.2 The Working Principle of the LS-TENG: the Coupling of 39 Dynamically Self-adjustable L-L Triboelectric Mechanism and 40 S-S CE

41 **Dynamically Self-adjustable L-L Contact Electrification (DSL-L  
42 CE).** In the soft liquid balloon, silicone oil and deionized water  
43 are employed as binary liquid electrodes due to their  
44 immiscibility. Although these two liquids contact each other at  
45 their interface (Figure 2a-i), they remain separate as distinct  
46 bulk phases. Under the impetus of water waves, the LS-TENG's  
47 operation results in dynamic interactions within the inner  
48 liquid balloon, where the two immiscible liquids interpenetrate  
49 each other's bulk phases. As depicted in Figure 2a-ii, this  
50 interpenetration forms numerous temporary biphasic droplets  
51 of varying sizes and irregular shapes. As these droplets of the  
52 two liquids come into contact, their interfaces experience  
53 relative displacements, generating triboelectric charges  
54 through triboelectrification at these transient contact  
55 interfaces.



**Figure 2.** The overall coupling process of the DSL-L CE and the S-S CE. a) Formation mechanism of the dynamically self-adjustable L-L interfaces and the corresponding DSL-L CE coupling with the S-S CE. b) COMSOL Multiphysics simulation results showing the potential distribution across the LS-TENG during operation. The figure is color-coded to represent the voltage ranges, and the overall voltage gradient in the figure is 0-196 V.

Due to the inherent tendency of the immiscible phases to separate and return to their equilibrium positions, the charged droplets undergo dynamic migration (Figure 2a-(iii-v)), which makes the triboelectric charges dynamically transfer along the copper core spring to the external circuit [48]. The situation of the corresponding open-circuit voltage (VOC) is shown in Figure S4. By this means, an electric potential difference between the two liquid phases is generated. Thus, the corresponding ISC is generated. The L-L CE and dynamic self-adjustment of the L-L contact interfaces between these binary mixed liquid electrodes significantly enhance the charge transfer capabilities of the LS-TENG device, effectively improving its efficiency in harvesting and utilizing wave energy. Figure 2b illustrates the potential distribution of the LS-TENG during the LS-TENG's operation simulated by using COMSOL Multiphysics.



**Figure 3.** The charge transfer mechanism of the silicone oil-H<sub>2</sub>O binary immiscible L-L interfaces and the S-S CE process between the self-adaptive

1 soft-contact interfaces (the cotton layer and the PI layer). a-b) The L-L CE  
2 and charge transfer mechanism based on the electron cloud potential-well  
3 model. a) Before the silicone oil-H<sub>2</sub>O contacting. b) Contacting. c) The CE  
4 charges separate and migrate during the L-L interfaces' contacting and  
5 relative displacement occurring. d) The self-adaptive, soft-contact S-S CE  
6 process

7 The charge transfer mechanism at the dynamic L-L interface  
8 is illustrated in Figure 3a-b. Before the contact of the two liquid  
9 phases (Silicone Oil - H<sub>2</sub>O molecules), the electrons could not  
10 transfer due to the local trapping effect of the potential wells  
11 (Figure 3a). When silicone oil contacts with H<sub>2</sub>O molecules, the  
12 electron clouds overlap, and the initial single potential well of  
13 their own becomes asymmetric double-well potential and then  
14 the electrons could hop from the atom of silicone oil to the  
15 atom of H<sub>2</sub>O molecules (Figure 3b). After hopping, the charges  
16 separate and migrate with the liquid phase moving (Figure 3c).

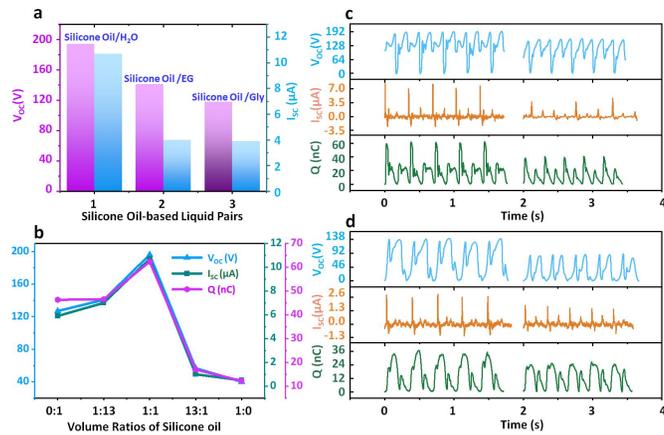
17 **Self-adaptive and Soft Contact S-S Triboelectric Effect.** Initially,  
18 without the push of external water waves, the liquid balloon is  
19 in a quiescent state (Figure 3d-i), retaining an ellipsoidal shape  
20 due to its gravity. However, when driven by the movement of  
21 water waves, the liquid balloon begins to swing back and forth,  
22 just like a moving pendulum, leading to the cotton layer  
23 repeatedly coming into contact (Figure 3d-ii) and separating  
24 (Figure 3d-iii) with the polyimide tape surface adhered to the  
25 inner surface of the hard acrylic spherical shell, and generating  
26 triboelectric charges at these two interfaces. During this  
27 dynamic process, the consequent real-time deformation of the  
28 soft liquid balloon appears. In an entire working cycle of the  
29 LS-TENG, self-adaptive and soft contact-separation processes  
30 occur alternatively between the polyimide tape adhered to the  
31 inner surface of the hard acrylic spherical shell and the cotton  
32 layer covered outside of the soft liquid balloon, significantly  
33 increasing the contact area compared with the traditional hard  
34 point contact manner, and consequently generating more  
35 triboelectric charges at the contact interfaces. Due to the  
36 periodic reciprocating movements of water wave energy, this  
37 self-adaptive and soft contact-separation mode proceeds also  
38 periodically. Moreover, this unique soft and self-adaptive  
39 contact-separation manner can significantly reduce mechanical  
40 wear and protect the LS-TENG from being structurally  
41 damaged caused by conventional hard point contact.

42 **The coupling of the above DSL-L CE and the S-S CE.** Based on  
43 the above discussion, here we propose a detailed DSL-L CE and  
44 the S-S CE coupling mechanism for the LS-TENG's working  
45 process: initially, the LS-TENG floats quietly on the surface of  
46 the water, with the soft liquid balloon suspended in the inner  
47 chamber of the hard acrylic spherical shell by the copper core  
48 spring. In this state, the liquid balloon could move along with  
49 the spherical shell. As we know, water waves provide both  
50 vertical lift and horizontal thrust movements due to the water  
51 particles' movement orbits in water waves. When a wave comes,  
52 the LS-TENG will be lifted and tilted by the buoyant force and  
53 water wave energy, making the inner liquid balloon convert the  
54 wave motion in the vertical direction into a lateral directional  
55 movement. As a water wave passes through the LS-TENG  
56 device, the mechanical energy of water waves could be

transferred to the LS-TENG, causing the lateral displacement  
and tilt of the LS-TENG device. Consequently, when the water  
waves drive the whole LS-TENG, the liquid balloon swings  
laterally within the shell to repeatedly contact and separate  
with the inner surface of the hard acrylic spherical shell. By this  
means, the unique soft contact and self-adaptive manner is  
realized, significantly increasing the S-S contact area between  
the two electrification layers, thus enhancing the energy  
harvesting efficiency and protecting the LS-TENG device from  
mechanical wear and damage. During the LS-TENG's working  
process, both the S-S and the L-L CE couple to significantly  
enhance the wave energy harvesting efficiency of the  
LS-TENG's

### 2.3 The Influence of DSL-L CE on the LS-TENG's output performance.

To evaluate the L-L influence of the triboelectric effect  
generated between the binary immiscible liquid electrodes  
inside the latex balloon on the output performance of the  
LS-TENG, firstly, we selected silicone oil in combination with  
three distinct liquids as the LS-TENG's liquid electrode,  
respectively, including deionized water, ethylene glycol (EG),  
and glycerol (Gly), to form three pairs of binary immiscible  
liquid electrodes. The volume ratio of the silicone oil in each  
liquid pair is kept identical. The corresponding LS-TENG's  
output performances from each kind of binary immiscible  
liquid electrode were measured. The results show that the  
electric output performance of LS-TENG with the pair of  
silicone oil-deionized water as the liquid electrode is the best  
compared with those of the other two kinds of liquid pair  
electrodes, as shown in Figure 4a. To study the reason why the  
LS-TENG with silicone oil-deionized water liquid electrode pair  
exhibits the optimal electrical output performance, we further  
employ the silicone oil-deionized water pair as the liquid  
electrode with different volume ratios (0:1, 1:13, 1:1, 13:1, and  
1:0) to test the LS-TENG's output performances. The result  
turns out that as the volume fraction of silicone oil in the binary  
mixture increases, the electrical output performance of the  
LS-TENG gradually boosts, including the  $V_{OC}$ ,  $I_{SC}$ , and charge  
quantity ( $Q$ ). However, this increasing trend does not persist all  
the time. As can be observed from Figure 4b, the optimal  
electrical output performance of the LS-TENG is achieved when  
the volume fraction of silicone oil reaches a 1:1 ratio.  
Subsequently, as the volume fraction of silicone oil continues to  
increase, the electrical output performance of the LS-TENG  
begins to decline.



1  
2 **Figure 4.** Further study and proof of the DSL-L CE mechanism. a) The  
3 LS-TENG's output performance comparison using different kinds of binary  
4 immiscible liquid pairs as the electrodes, including silicone oil-water,  
5 silicone oil-EG, and silicone oil-Gly. b) Optimizing the LS-TENG's output  
6 performance by using the silicone oil-water liquid pair as the electrode, in  
7 which the volume ratios of the silicone are 0:1, 1:13, 1:1, 13:1, and 1:0,  
8 respectively. c) The comparison of the LS-TENG's output performances,  
9 respectively, from the silicone oil-water pair (immiscible) and the  
10 Gly-water pair (miscible) as the liquid electrodes. d) The comparison of the  
11 LS-TENG's output performances, respectively, from the silicone oil-EG pair  
12 (immiscible) and the glycerin-ethylene glycol pair (miscible) as the liquid  
13 electrodes.

14 According to the above comparison results, one of the critical  
15 factors affecting LS-TENG's output performance should be  
16 attributed to the contact area between the two immiscible  
17 liquid phases. Compared to water, either ethylene glycol or  
18 glycerol forms a more cohesive mixture with silicone oil due to  
19 their inherently high viscosities, leading to the two phases  
20 being practically inseparable and unable to generate  
21 substantial dynamic separable L-L interfaces. In contrast, water  
22 is completely immiscible with silicone oil and has a lower  
23 viscosity. As a result, under the mechanical driving of ocean  
24 waves on the LS-TENG, a substantial number of temporary  
25 dynamic interfaces are formed between the silicone oil and  
26 water phases. These dynamic and self-adjustable L-L interfaces  
27 are continuously created and subsequently dissipated with the  
28 periodic mechanical driving of the water waves due to the  
29 natural phase separation of water and silicone oil. This  
30 constant process of contact and separation at these dynamic  
31 L-L interfaces generates triboelectric charges at the silicone oil  
32 and deionized water interfaces. Moreover, the significant  
33 difference in electrical conductivity between water and silicone  
34 oil leads to a potential difference between these interfaces  
35 upon their separation. According to the working mechanism of  
36 the contact-separating mode triboelectric nanogenerator, the  
37 triboelectric charges between the water and silicone oil  
38 interfaces are then transferred to the outer circuit,  
39 substantially enhancing the electrical output performance of  
40 the LS-TENG.

41 The 1:1 volume ratio of silicone oil to deionized water  
42 demonstrates the highest electrical output performance. The  
43 possible reason, we think, is that at 1:1 volume ratio of silicone  
44 oil to deionized water maximizes the contact area between the  
45 two immiscible liquids. At equal proportions, both liquids are

able to form a balanced and widespread interface within the confined space of the LS-TENG's soft balloon. This balanced ratio allows both liquids to interact more extensively with each other, leading to the creation of numerous transient L-L interfaces as the balloon moves during operation. At other volume ratios (e.g., 1:3 or 3:1), one liquid dominates, reducing the effective contact area between the two phases. When one liquid occupies more space, the opportunities for interaction between the liquids are limited, leading to fewer dynamic L-L contact interfaces and, therefore, reduced triboelectric charge generation. In contrast, at the 1:1 ratio, the two immiscible liquids are evenly distributed, which maximizes their interaction as they repeatedly contact and separate. This increases the efficiency of the charge transfer process and enhances the overall electrical output performance of the LS-TENG. In essence, the 1:1 ratio optimizes the mechanical interaction and dynamic phase separation, ensuring a higher generation of triboelectric charges, which is why it results in better electrical output performance.

To confirm our proposed DSL-L CE mechanism, we further conducted a series of control experiments as follows. Four pairs of binary liquid electrodes were adopted, including (i) silicone oil-deionized water (Immiscible), (ii) glycerin-deionized water (Miscible), (iii) silicone oil-ethylene glycol (Immiscible), and (iv) glycerin-ethylene glycol (Miscible). As shown in Figure 4c, the left-side curves in this figure exhibit the LS-TENG's output performances from the silicone oil-deionized water pair as the liquid electrode (pair (i)), and the corresponding right-side curves show those of the glycerin-deionized water as the liquid electrode (pair (ii)). Similarly, the left side curves in Figure 4d give the LS-TENG's output performances from the silicone oil-ethylene glycol pair as the liquid electrode (pair (iii)), and the curves on its right side belong to those of the glycerin-ethylene glycol as the liquid electrode (pair (iv)). Obviously, the output performances shown on the left sides in Fig. 4c-d are all higher than those on the right sides, which means that the binary immiscible liquid electrodes endow the corresponding LS-TENG with better electric output performances than the binary miscible liquid electrodes do. Furthermore, the electric output performances of the LS-TENG from the silicone oil-deionized water pair (Immiscible) as the liquid electrode are better than those of the glycerin-deionized water pair (miscible) as the liquid electrode.

The results of these control experiments support the validity of the above-proposed DSL-L CE mechanism. Specifically, driven by the external water wave energy, the binary immiscible liquid electrodes within the LS-TENG form numerous dynamically self-adjustable L-L interfaces that significantly increase the L-L contact area of the LS-TENG, thus greatly enhancing the generation of triboelectric charges at the L-L interfaces. The formed transient, abundant dynamic L-L interfaces separate due to the phase separation of the immiscible liquid phases, thereby disrupting the symmetry of the positive and negative charges generated within the liquid electrodes. As a result, the generated positive and negative triboelectric charges do not neutralize each other due to geometric symmetry but are instead carried along with the L-L phase separation to the external circuit. This process effectively enhances the electrical output performance of the LS-TENG.

In contrast, in the binary miscible liquid electrode systems

1 (such as pair (ii) and (iv)), where two liquids mix to form a  
 2 uniform, stable single phase, no L-L interfaces are formed.  
 3 Consequently, in the LS-TENGs utilizing these miscible binary  
 4 liquids as electrodes, there is no generation of L-L interface  
 5 triboelectricity, and the triboelectric charge generation occurs  
 6 only through the S-S contact-separation between the external  
 7 cotton layer covered on the soft liquid balloon and the inner  
 8 surface of the external hard acrylic spherical shell. This feature  
 9 distinguishes them significantly from systems where  
 10 immiscible binary liquid electrodes create dynamic interfaces  
 11 that enhance triboelectric effects.

#### 12 2.4 Further Verification of the DSL-L CE and Optimization of 13 the LS-TENG's Output Performance.

14 To further verify the dynamic triboelectric charge generation at  
 15 the L-L interface of silicone oil-deionized water, we designed a  
 16 validation experiment detailed in Figure 5a, in which we  
 17 utilized a disposable infusion needle connecting with an  
 18 infusion bottle to make the deionized water droplet fall  
 19 downward to contact with the silicone oil layer covered on the  
 20 bottom of the petri dish. By adjusting the roller on the infusion  
 21 tube, the falling speed and frequency of the deionized water  
 22 droplet could be controlled uniformly.

23 It's worth noting that a layer of copper tape was pre-attached  
 24 to the bottom of the Petri dish as the electrode. The distance  
 25 between the infusion needle and the surface of the silicone oil  
 26 layer is precisely adjusted to ensure that each water droplet  
 27 falling from the needle could be just in contact with the surface  
 28 of the bottom silicone oil layer and, at the same time, does not  
 29 break away from the tip of the needle. To avoid the previously  
 30 fallen water droplets staying and directly spreading out on the  
 31 surface of the silicone oil right below the tip of the needle, thus  
 32 causing interference to the subsequent falling water droplets,  
 33 the Petri dish is consequently inclined at a slight angle to allow  
 34 each drop falling from the tip of the needle immediately to slide  
 35 down the inclined silicone oil surface as soon as it touches the  
 36 silicone oil surface.

between the L-L interface of silicone oil-water. b) The L-L CE process at the  
 L-L interfaces of the silicone oil-water. c) The dynamic triboelectric signal  
 of L-L CE was detected. d) The optimal matching resistance is determined  
 at the intersection of the two curves. e) The curves of charging different  
 capacitors by using the LS-TENG. f-h) The maximum electric output  
 performances: f) current (I), g) transfer charges (Q), and h) voltage (V).

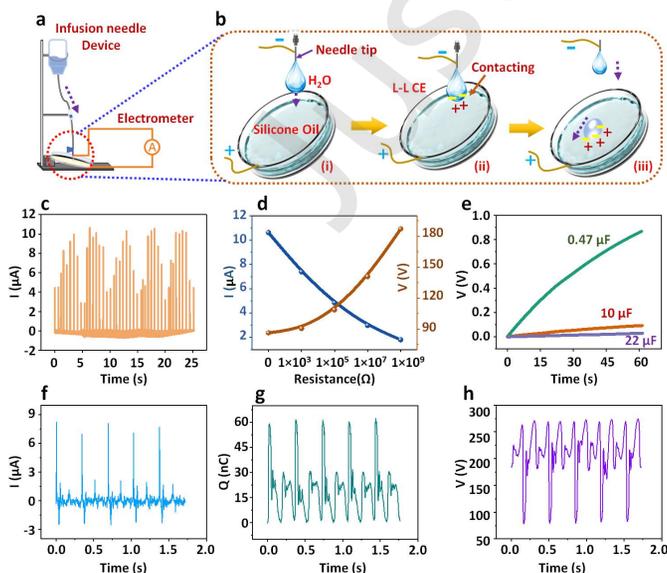
By this method, a double-electrode mode TENG is  
 constructed, as shown in Figure 5b. Once the water droplets  
 from the tip of the needle come into contact with the surface of  
 the silicone oil, an L-L CE occurs on their contact surfaces. In  
 this continuous dynamic process, a potential difference is  
 generated at the interface of silicone oil and water, and the  
 corresponding voltage signals of the triboelectric effect are  
 measured by connecting the positive and negative terminals of  
 an electrostatic meter to the copper tape of the Petri dish and  
 the needle, respectively, as depicted in Figure 5c. The result of  
 this control experiment confirms our proposed DSL-L CE  
 mechanism.

To enhance the conversion of mechanical energy into  
 electrical energy by the LS-TENG and reduce energy losses  
 during this process, we assess the impedance matching of the  
 LS-TENG. As shown in Figure 5d, we connect resistors of  
 varying values in series with the LS-TENG and record the  
 current and voltage values with the values of the  
 corresponding load resistance, and the optimal resistance is  
 determined at the intersection of the two curves. Additionally,  
 we tried to use the LS-TENG to charge capacitors of  $0.47\mu\text{F}$ ,  
 $10\mu\text{F}$ , and  $22\mu\text{F}$ , respectively. The corresponding charging  
 curves are depicted in Figure 5e. Besides, the maximum output  
 performances of the LS-TENG are obtained, shown in Figure 5  
 f-h.

#### 2.5 All-weather and real-time monitoring for Marine IoT sensor

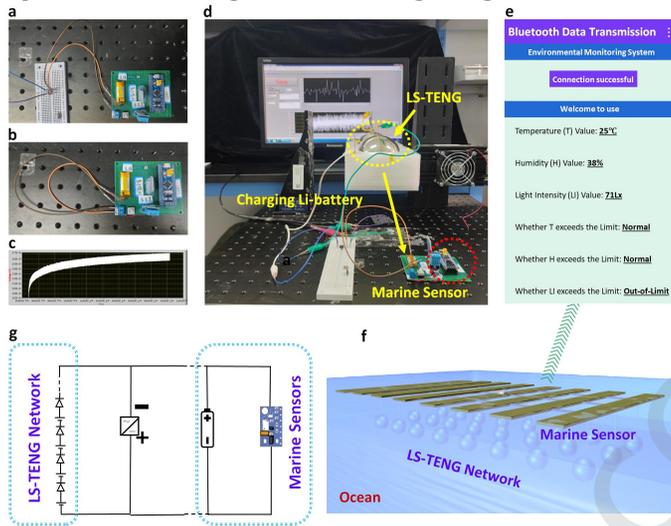
The marine environment, a complex and dynamic ecosystem,  
 presents numerous hazards, especially due to its unpredictable  
 weather conditions, such as storms, hurricanes, and strong  
 currents that pose significant risks to operation at sea. To  
 address these challenges, we have implemented real-time  
 monitoring using all-weather sensors that can not only ensure  
 the safety of operation at sea but also help marine  
 meteorological analysis and forecasting. This sensing system  
 tracks environmental parameters like temperature, humidity,  
 and light intensity, with data visualized through a mobile app,  
 as displayed in Video S1.

To realize marine environmental monitoring, the sensor  
 systems employed typically operate on 3.7 V lithium batteries.  
 However, due to the limited lifespan of these batteries, they  
 require frequent replacements after certain periods of  
 operation. This replacement process inevitably interrupts the  
 sensor device's working, preventing continuous, real-time,  
 all-weather monitoring. In this work, all-weather and real-time  
 marine environment monitoring is achieved by continuously  
 collecting ocean wave energy by the LS-TENG. The LS-TENG  
 (Figure 6a) effectively charges the adopted lithium battery,  
 which harnesses energy from ocean wave movements. By this  
 means, the ocean wave energy is initially stored in the lithium  
 battery and then converted into direct current (DC) to power  
 the sensor system using a rectifier (Figure 6b), which not only



37  
 38 **Figure 5.** Further verify the dynamic triboelectric charge generation  
 39 between the silicone oil-water L-L interfaces and optimize the LS-TENG's  
 40 output performance. a) The dynamic triboelectric charge generation

1 powers the sensor system but also ensures a continuous and  
 2 stable power supply under varying environmental conditions,  
 3 as evidenced by the charging curve observed during the  
 4 charging process (Figure 6c). Additionally, laboratory  
 5 simulations of marine environments were conducted using  
 6 linear motors to mimic ocean wave motions. These simulations  
 7 facilitated optimizing the LS-TENG's performance by  
 8 fine-tuning parameters such as speed and acceleration to  
 9 closely match the natural frequencies of ocean waves, as  
 10 demonstrated in Figure 6d and Video S2. For broader  
 11 applications, the LS-TENG could be scaled up into a distributed  
 12 network to increase energy harvesting capabilities from ocean  
 13 wave movements (Figure 6e-f), ensuring the sensors' reliable  
 14 operation across all weather conditions, as detailed in the  
 15 equivalent circuit diagram shown in Figure 6g.



16  
 17 **Figure 6.** Powering the marine IoT sensor to realize all-weather and  
 18 real-time monitoring for marine environmental monitoring. a) The lithium  
 19 battery of the marine sensor is charged by the LS-TENG. b) The  
 20 LS-TENG-charged lithium battery to power the marine sensor. c) The  
 21 charging curve during the lithium battery charging process. d) Simulating  
 22 marine environments to mimic ocean wave motions to optimize the  
 23 LS-TENG's output performance. e-g) The schematic of the scaled-up  
 24 LS-TENG into distributed networks to enhance energy harvesting  
 25 capabilities from ocean waves: e) The mobile app showing the sensing  
 26 results of the marine environmental monitoring. f) The schematic of the  
 27 LS-TENG networks. g) The equivalent circuit diagram of the marine sensor  
 28 powered by the LS-TENG.

### 29 3. Conclusion

30 In this work, an LS-TENG is designed to harvest water wave  
 31 energy. The novel ellipsoidal, pendulum-like structure of the  
 32 LS-TENG integrates both L-L and S-S triboelectric couplings.  
 33 Firstly, the binary immiscible liquid electrodes in the inner soft  
 34 balloon provide plenty of dynamic, self-adjustable L-L contact  
 35 interfaces, significantly increasing the L-L contact area, thus  
 36 enhancing the L-L CE and improving wave energy harvesting  
 37 efficiency. Secondly, the unique self-adaptive, soft contact  
 38 manner substantially increases the S-S contact area, which  
 39 efficiently overcomes the limitation of the traditional  
 40 solid-solid interface's point-point hard contact and makes the  
 41 LS-TENG better adopt the irregular motions of water waves,  
 42 not only enhancing the energy harvesting efficiency but

protecting the TENG from mechanical wear and damage. The  
 unique structure of the LS-TENG provides an innovative and  
 effective way of collecting water wave energy. More importantly,  
 the continuous marine environment sensor is successfully  
 powered by the LS-TENG to realize all-weather and real-time  
 marine environment monitoring, including temperature,  
 humidity, and light intensity.

## 4. Experimental section

### 4.1 Fabrication of the Outer Hard Spherical Shell

First, two acrylic hemispherical shells with a diameter of 10 cm  
 and a thickness of 0.21 cm are utilized. The clean inner shell is  
 then uniformly coated with a silver layer by magnetron  
 sputtering at 70W for 1200 s. Then, a polyimide film is carefully  
 covered on the silver layer.

### 4.2 Preparation of the Inner Soft Liquid Balloon

A latex balloon, a polyurethane (PU) wrapped Cu-core spring,  
 cotton, silicone oil, and deionized water were prepared. The  
 binary immiscible silicone oil-water was injected into the latex  
 balloon via a syringe. One end of the Cu-spring is inserted into  
 the water phase of the liquid system of the balloon while its  
 other end is led outside of the balloon. The liquid-filled balloon  
 is then sealed, and a cotton layer is adhered to the balloon's  
 exterior with a PVP solid adhesive.

### 4.3 LS-TENG's Assembly

A small hole slightly smaller than the Cu-spring's diameter is  
 drilled into the prepared hard acrylic shell. The Cu-spring goes  
 through the hole to the outside of the hard shell. Finally, the  
 gaps between the Cu-spring and the hard shell are sealed via a  
 hot melt adhesive (ethylene-vinyl acetate copolymer, EVA).

### 4.4 Measurement of output voltage and current:

To measure the triboelectric charge generation, we used the  
 Keithley 6514, a high-precision electrometer, to capture the  
 output voltage and current generated by the LS-TENG. The  
 electrometer was connected to the external circuit of the  
 LS-TENG, allowing real-time measurement of electrical output  
 under different operational conditions, such as varying wave  
 frequencies.

**a) Voltage measurement:** The electrometer was used to record  
 the peak open-circuit voltage generated by the LS-TENG,  
 ensuring accurate and consistent data collection. The high  
 sensitivity of the electrometer allowed us to detect even small  
 voltage fluctuations during operation.

**b) Current measurement:** Similarly, the electrometer measured  
 the short-circuit current, which reflects the triboelectric charge  
 transfer occurring between the L-L and S-S interfaces.

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**Electronic Supplementary Material:** Supplementary material (the optical image and the preparation of the LS-TENG device; the SEM images of the polyimide dielectric layer surface after different working periods, and the overall coupling process of the DSL-L CE and the S-S CE) is available in the online version of this article at <https://doi.org/10.26599/NR.2025.94907052>.

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*Just Accepted*

## Electronic Supplementary Material

# Dynamically self-adjustable liquid-liquid and self-adaptive soft-contact solid-solid triboelectric nanogenerator for wave energy harvesting

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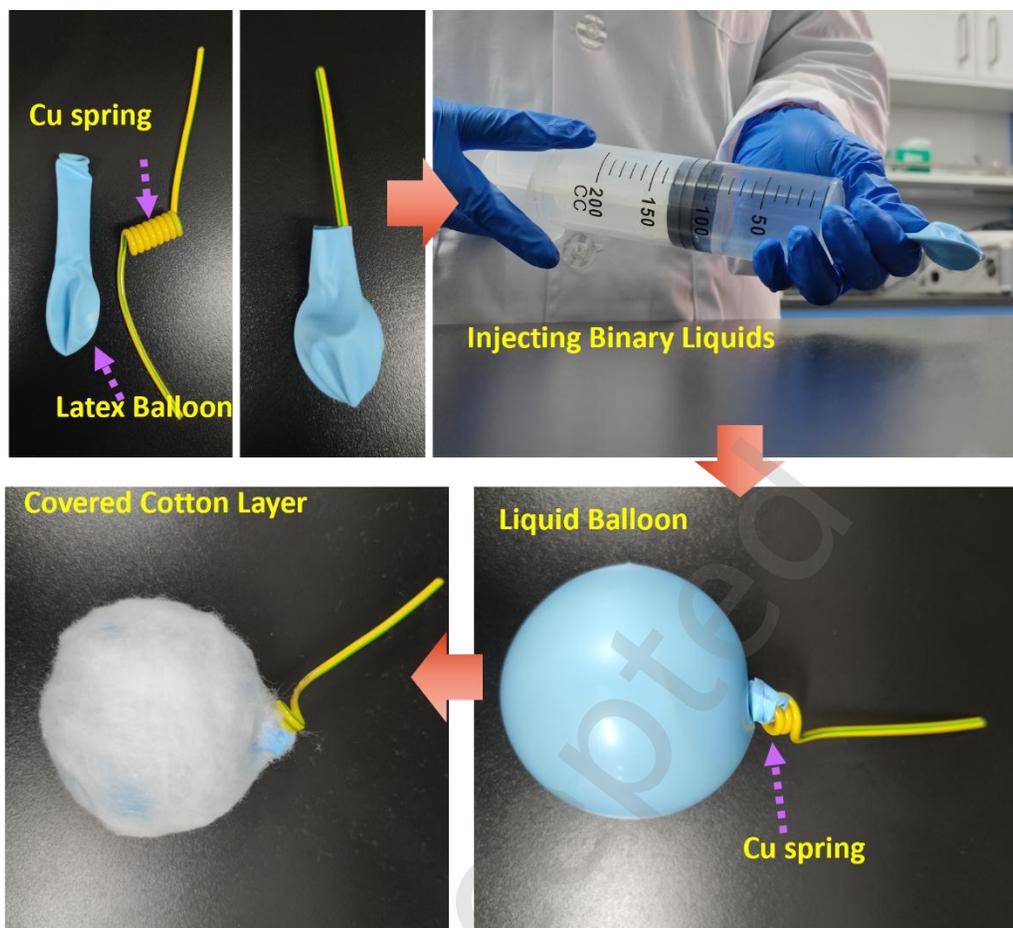
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<sup>§</sup> Yong Long and Bingqi Zhao contributed equally to this work.

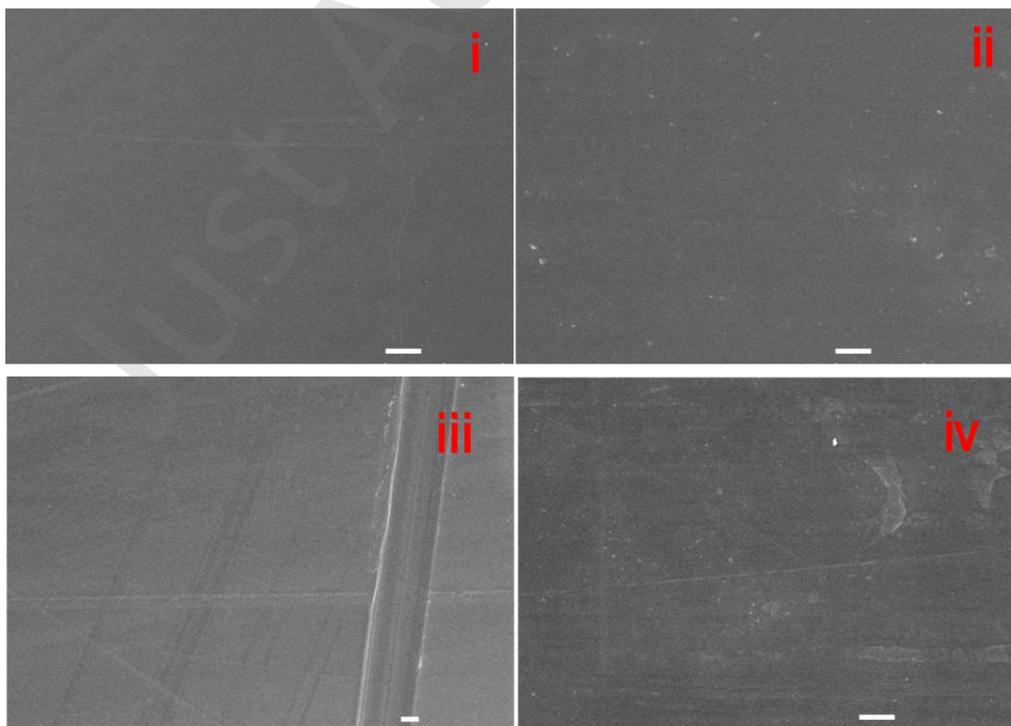
Supporting information to <https://doi.org/10.26599/NR.2025.94907052>



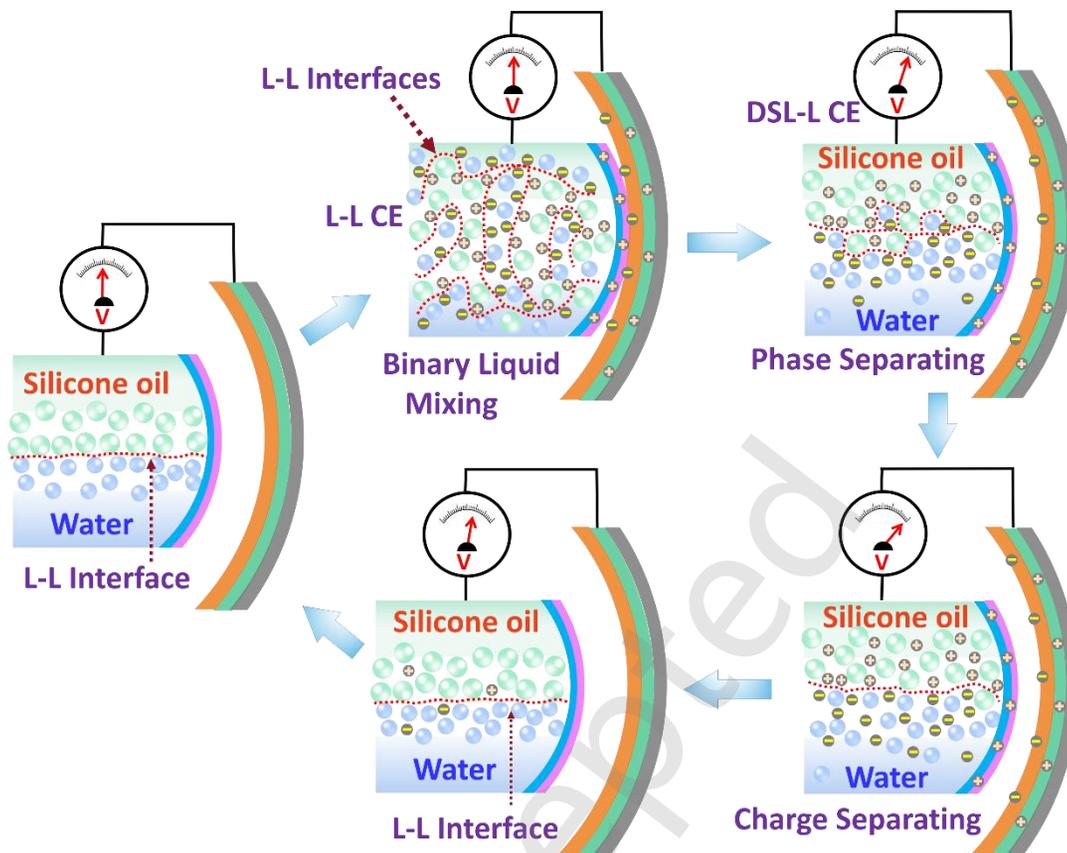
**Figure S1.** The optical image of the LS-TENG device.



**Figure S2.** The preparation process of the internal soft liquid balloon of the LS-TENG.



**Figure S3.** SEM images of the polyimide dielectric layer surface after different working periods (0 h, 6 h, 12 h, and 48 h), demonstrating little mechanical wear on the contact surfaces and effectively extending the TENG's working longevity.



**Figure S4.** The overall coupling process of the DSL-L CE and the S-S CE. a) The output performance of Voc of the LS-TENG during the DSL-L CE and coupling with the S-S CE.